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Invited review

A review of shale pore structure evolution characteristics with increasing thermal maturities

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Abstract:

Pore structure has a significant effect on the occurrence state of shale hydrocarbons and the hydrocarbon storage capability of shale reservoirs. Consequently, it is quite meaningful to clarify the shale pore structure evolution characteristics for understanding the migration and enrichment mechanisms of hydrocarbons within shale reservoirs during different geological stages. The abundant existence of organic matter within shales complicates the shale pore structure evolution process by hydrocarbon generation, migration and cracking. Many studies have been conducted to reveal the shale pore structure evolution characteristics and the controlling factors. Basically, these studies could be divided into two categories based on the sample source: comparing the pore structure of natural shale samples with different thermal maturities; obtaining shale samples with different thermal maturities by conducting thermal simulation experiments on low-mature shale samples and comparing the pore structure of these simulated shale samples. However, no consistent viewpoint on shale pore structure evolution has been reached. This review presents the state of the art of shale pore structure evolution studies. It is widely recognized in the literature that both the inorganic and organic diagenesis control the shale pore structure evolution process. However, it is found that the shale pore structure evolution models proposed in the literature were largely dependent on the samples used. And it is recommended to conduct the two categories of studies simultaneously in order to obtain more reliable shale pore structure evolution characteristics in future investigations.

1. Introduction

Shale hydrocarbons have been considered as one of the most promising unconventional petroleum resources since the economic production of shale gas in North America with the development of hydraulic fracturing and horizontal drilling technologies more than twenty years ago (Curtis, 2002). Many countries, such as United States, Canada and China, have made important breakthroughs in shale gas/oil exploration and the studies focusing on the unconventional petroleum geology and engineering are booming in recent years (e.g., Zhao et al., 2007; Ross and Bustin, 2008; Zou et al., 2010; Dai et al., 2014; Klaver et al., 2015; Pan et al., 2016; Wood and Hazra, 2018; Liu et al., 2019; Wood, 2019; Yang et al., 2020). Among these studies, reservoir characterization is regarded as one of the core research contents in unconventional petroleum geology (e.g., Loucks et al., 2009; Chalmers et al., 2012; Clarkson

et al., 2013; Milliken et al., 2013). Organic-rich shales deposited in fine-grained sedimentary system usually underwent complicated diagenesis with the participation of organic fluids generated during the thermal evolution process of organic matter and finally oil/gas was distributed in pore spaces of shale reservoir either in free state, adsorbed state or dissolved state (Curtis, 2002; Ross and Bustin, 2007). Consequently, shale pore structure, which has experienced an intense and multi-stage transformation process and is more complicated than conventional reservoir rocks, has an important impact on hydrocarbon storage capability of shale reservoir (Ross and Bustin, 2009; Rexer et al., 2014).

In order to evaluate the reserve of shale hydrocarbons and predict the oil/gas production behavior accurately, it is quite meaningful to clarify the occurrence state of shale hydrocarbons and its controlling factors. Free gas/oil is easier to be

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produced without desorption process but adsorbed phase may provide huge amount of hydrocarbons in a long term if treated properly (Curtis, 2002). Shale pore structure is considered as one of the most important reservoir parameters controlling occurrence state of hydrocarbons (Curtis et al., 2010; Slatt and O'Brien, 2011; Chen and Xiao, 2014). Total pore volume and specific surface area are the two pore structure parameters determining the storage potential of free and adsorbed gas/oil in shale reservoirs respectively. Furthermore, the proportion and development characteristics of oil-wet organic matter (OM) pores and water-wet inorganic pores also affect the occurrence state of hydrocarbons significantly. Consequently, many studies have been conducted to investigate the shale pore structure from qualitative description to quantitative characterization using advanced tools including high pressure mercury intrusion porosimetry (HPMIP), N₂/CO₂ adsorption, field emission-scanning electron microscopy (FE-SEM), focused ion beam-scanning electron microscopy (FIB-SEM), nuclear magnetic resonance (NMR), nanometer-computed tomography (Nano-CT) and small-angle scattering (Clarkson et al., 2012; Javadpour et al., 2012; Loucks et al., 2012; Kuila and Prasad, 2013; Milliken et al., 2013; Bahadur et al., 2015; Zhou and Kang, 2016; Gao and Hu, 2018). The widely used pore classification standard proposed by the International Union of Pure and Applied Chemistry (IUPAC) is that micropores (<2nm), mesopores ($2 \sim 50$ nm) and macropores (>50 nm) (Sing et al.,1985).

Total organic carbon (TOC) content, kerogen type, shale mineralogy and thermal maturity are generally considered as the main controlling factors of shale pore structure in the literature (e.g., Jarvie et al., 2007; Loucks et al., 2012; Mastalerz et al., 2013; Löhr et al., 2015). And it is quite meaningful to clarify how the shale pore structure changes with thermal maturity for understanding the evolution process of shale hydrocarbon occurrence state during different geological stages and the enrichment mechanism of shale hydrocarbons. However, it should be point out that most studies focused on the 'static' pore structure characterization and few studies were conducted to show a 'dynamic' pore structure evolution process. Furthermore, the limited studies focusing on shale pore structure evolution characteristics always showed different viewpoints on the function of OM, brittle minerals, clay minerals and their interactions in shale pore structure evolution. Basically, the studies on shale pore structure evolution could be divided into two categories based on the sample source: (1) comparing the pore structure of natural shale samples with different thermal maturities; (2) obtaining shale samples with different thermal maturities by conducting thermal simulation experiments on low-mature shale samples and comparing the pore structure of these simulated shale samples. This review presents the state of the art of shale pore structure evolution studies in these two categories.

2. Natural shale samples with different thermal maturities

Jarvie et al. (2007) found a porosity increase with increasing thermal maturity when they conducted a thermogenic shale-gas assessment study on the Mississippian Barnett Shale of north-central Texas and attributed this phenomenon to the thermal conversion of kerogen to petroleum but no further investigation was conducted on shale pore structure evolution.

Based on the collected data of mudrocks from 26 geologic units (from Cambrian to Pliocene-Pleistocene), Loucks et al. (2012) classified the pores in mudrocks into three types including interparticle and intraparticle pores associated with mineral particles as well as OM pores and they described the pore structure characteristics of each type and discussed their origins in details. Furthermore, they presented a preliminary discussion on the evolution of mudrock pores with time and burial. Mechanical compaction, which causes a great loss of interparticle and intraparticle pores, is the most important process during the early history of burial with limited carbonate, phosphate, and early pyrite diagenesis (Raiswell, 1976; Föllmi, 1996; Wilkin et al., 1996, 1997). With the increase of burial depth and temperature (e.g., >100 °C), the transformation of smetite to illite occurs commonly and the pore space could be filled with the new authigenic clays and minerals formed using the released elements (e.g., silica, calcium and so on) from this transformation process (Freed and Peacor, 1989; Pearce et al., 1991; Hatch, 2012). In the burial temperature range of 80-120 °C, dissolved pores could be produced by the dissolution of unstable carbonates and feldspars, which is caused by the carboxylic and phenolic acids generated from the decarboxylation of kerogen. Loucks et al. (2012) also pointed out OM pores began to form with the start of organic thermal maturation but no linear correlation between OM pore development and increased maturation was observed in Barnett Shale samples covering a range of vitrinite reflectance (R_0) values (0.5%~3.17%). Basically, Loucks et al. (2012) mentioned most of the diagenesis processes involved in the pore structure evolution of shale samples and briefly showed the development situation of three pore types in different diagenetic stages. However, the main objective of their study was not clarifying the pore structure evolution process of shale samples and no specific pore structure evolution model was established by Loucks et al. (2012).

Considering the significant impact of OM pores on the storage and production of shale hydrocarbons, Curtis et al. (2012) conducted a tentative investigation on the development of organic porosity with increasing thermal maturity using eight Woodford Shale samples from Oklahoma in USA with a mixture of type II and III kerogen and Ro values ranging from 0.51% to 6.36%. By setting thresholds on the gray scale of SEM images, they obtained the OM content and organic porosity of each sample. It was found OM content in the milled sample areas decreased with the increase of thermal maturity, which was possibly due to the limited observation area in each SEM image or thermal alteration and compaction of OM. However, no systematic evolution trend was observed in the organic porosity with increasing thermal maturity. More specifically, no OM pores were found in shale samples with 0.9% R_o and below while OM pores were quite well-developed in shale samples with 1.23% R_o and above (except 2.0% R_o sample). Furthermore, based on the observation of no organic porosity in 2.0% Ro sample and the co-existence of porous

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and non-porous OM within less than a micron domain in 1.4% R_o sample, they concluded thermal maturity was not the only factor controlling the development of OM pores and other factors such as organic matter composition should also be considered. It should be noted that the mineral compositions of these eight Woodford Shale samples were not provided and their possible effects on the OM pore structure evolution were not discussed by Curtis et al. (2012).

Milliken et al. (2013) investigated the OM pores developed in Marcellus Formation samples from two wells with different thermal maturities (~1.0% Ro and~2.1% Ro respectively) in northern Pennsylvania. One of their main findings was the controlling effect of total organic carbon (TOC) not thermal maturity on the development of OM pores, which was inconsistent with previous studies. After plotting porosity versus TOC, samples from each well exhibited a linear trend line and these two trend lines showed different intersections but similar slopes, which indicated the controlling effect of TOC on porosity and the similar OM porosity developed in these samples with two different thermal maturities. More specifically, they found a positive correlation between TOC and porosity for samples with TOC less than 5.5 wt% while this positive correlation vanished in samples with higher TOC. Furthermore, visible OM porosity under FE-SEM decreased with increasing TOC and the morphology and OM pore size also showed systematic variations with TOC. As to the causing mechanism of this 'surprising' result, they postulated that higher TOC might have greater OM connectivity and generate a more effective pathway for gas expulsion leading to the compaction of shale matrix and squeezing of OM pores. Milliken et al. (2013) pointed out OM type difference between samples with higher and lower TOC could also cause their different OM pore structures. However, the significant impact of thermal maturity on shale pore structure evolution could not be excluded considering the samples with only two different thermal maturities used by Milliken et al. (2013).

In order to clarify shale pore structure evolution process with increasing thermal maturity, a systematic shale pore structure characterization of Devonian and Mississippian New Albany Shale samples with marine type II kerogen and a Ro value range from 0.35% to 1.41% was conducted by Mastalerz et al. (2013). Low-pressure gas (N₂ and CO₂) adsorption, mercury intrusion porosimetry (MIP) and helium porosimetry(HP) were conducted to quantitatively characterize the whole-aperture pore size distribution of shale samples. As mentioned by Mastalerz et al. (2013), the well-documented coal-specific knowledge about the pore structure evolution of macerals with increasing coal rank was probably insufficient to reveal shale pore structure evolution process due to the possible and unique impacts of hydrocarbon generation, cracking, and formation of solid bitumen on pore structure in shale samples (Jarvie et al., 2007; Loucks et al., 2009; Curtis et al., 2011), which also confirmed the significance of Mastalerz et al. (2013)'s work. The results of organic petrography analysis showed different TOC contents and compositions of these samples. The distribution characteristics of OM and pores larger than 1 μ m observed under reflected light microscopy showed considerable differences among these samples with different thermal maturities and the interconnection of OM network seemed to be optimized gradually with the increase of thermal maturity. A nonlinear and trough-shaped trend between total pore volume and thermal maturity was indicated by both HP and MIP results and late mature sample IL-5 $(1.15\% R_0)$ had the lowest pore volume. More specifically, the changing tendency of micropores, mesopores and macropores with increasing thermal maturity was discussed separately by Mastalerz et al. (2013). The micropore volume and mesopore volume were quantified by CO₂ adsorption and N₂ adsorption respectively while the macropore volume was obtained by subtracting micropore volume and mesopore volume from HP total pore volume. Both the micropore volume and mesopore volume decreased first with increasing thermal maturity to a minimum in sample IL-5 (1.15% Ro) and then increased again for sample IL-1 (1.41% Ro) while this trend was not obvious for macropores. Furthermore, the BET surface area derived from N₂ adsorption, average micropore size derived from CO₂ adsorption, total pore area and median pore-throat diameter obtained from MIP all reached a minimum in sample IL-5 $(1.15\% R_0)$. Different from the viewpoint of Milliken et al. (2013), no obvious correlation between the total pore volume and TOC was observed by Mastalerz et al. (2013), which may be masked by the strong differences in thermal maturity. The lack of correlation between pore volume and TOC may also indicate the significant contributions of both interparticle pores and intraparticle pores to the pore spaces of these samples. In addition, Mastalerz et al. (2013) also pointed out the influences of different minerals on porosity were masked by the strong influence of thermal maturity and the micropore volume was mainly provided by OM and clay minerals. Finally, a systematic and classic shale pore structure evolution model with 4 stages was proposed by Mastalerz et al. (2013). Stage I $(R_o < 0.55\%)$: the total pore volume decreased a lot with the increase of thermal maturity due to the strong compaction. Stage II $(0.55\% < R_0 < 0.65\%)$: the total pore volume increased a little with the increase of thermal maturity due to the primary cracking of OM. Stage III ($0.65\% < R_0 < 1.15\%$): the total pore volume decreased again with the increase of thermal maturity due to the oil filling and solid bitumen formation, which was approved by the significant pore volume increase of sample IL-5 (1.15% R_0) after dichloromethane extraction. Stage IV $(R_0 > 1.15)$: the total pore volume increased again with the increase of thermal maturity due to the secondary cracking of OM. However, the monotonous increasing trend of pore volume after R_o>1.15 was probably not the case and the thermal maturity values at which the changing tendency of the pore volume reversed were disputable (Liu et al., 2017). Although this model was not perfect and more relevant studies were required to improve it, Mastalerz et al. (2013) indeed presented a representative methodology of investigating shale pore structure and its evolution process

The OM pore structure evolution characteristics of overmature shales were discussed by Wang et al. (2013). For shale samples with comparable TOC content ($2\% \sim 3\%$), the Lower Cambrian Qiongzhusi Formation shale samples with higher thermal maturity ($2.5\% \sim 2.8\%$ equivalent vitrinite reflectance R_{equ}) had lower porosities ($2\% \sim 3\%$) compared with the Upper Ordovician-Lower Silurian Longmaxi Formation shale samples with 2.0%~2.3% R_{equ} and 5%~7% porosity, both of which were collected from the Sichuan Basin in China. Consequently, Wang et al. (2013) pointed out the increasing trend of OM porosity with increasing thermal maturity ceased at 2.0% R_o and the OM porosity began to decline when thermal maturity was above 2.0% R_o . Furthermore, the preservation conditions of pore spaces also significantly controlled the development of OM porosity. Wang et al. (2013) also pointed out the matrix porosity of shale continued to decrease with increasing thermal maturity.

Focusing on the structure of OM in Barnett Shale samples with a series of thermal maturities from immature to wet-gas stage, Sarmiento et al. (2014) used N₂ adsorption method and high resolution transmission electronic microscopy (HRTEM) to characterize the pore volume and nanostructure of isolated kerogens respectively. The results of N2 adsorption showed that both the mesopore volume and BET surface area of isolated kerogens from different Barnett shale samples increased with increasing thermal maturity. The HRTEM images directly showed the existence of micropores and mesopores in these isolated kerogens. In immature isolated kerogens with a quasiamorphous structure, micropores were considered to result from the quasi-random orientation of aromatic layers (<1 nm). In gas-mature isolated kerogens, mesopores (2-50 nm) resulted from the disorientation of abundant basic structural units formed by stacking of larger aromatic layers (>1 nm) and the disorientation of molecular orientation domains formed by parallel arrangement of the basic structural units. Furthermore, the carbon nanoparticles of concentric nanostructure were observed within gas-mature samples by HRTEM and were possibly generated by secondary cracking of hydrocarbons (Alfe et al., 2009). However, no specific OM pore structure evolution model was established by Sarmiento et al. (2014).

The evolution of porosity and pore types in Lower Toarcian Posidonia Shale samples from the Lower Saxony Basin in North Germany was characterized by Mathia et al. (2016). A total of 26 samples with a R_0 value range of $0.53\% \sim 1.45\%$ were used and these samples mainly consisted of microfossiferous calcite, clay minerals and type II OM. The porosities of immature samples, oil-windows samples and gas-window samples were $10\% \sim 14\%$, $3\% \sim 5\%$ and $9\% \sim 12\%$ respectively and the evolution of porosity was generally following the model proposed by Mastalerz et al. (2013). The shale compositions, carbonate diagenesis, compaction and thermal evolution of organic phases were considered to be the main controlling factors of porosity changes at different thermal maturities. Furthermore, the heterogeneity of OM porosity was confirmed by the wide macroporosity range $(0 \sim 40\%)$ of different individual organic particles and the fact that no macropores were developed in 65% of the total organic particles. The physicochemical differences among different organic particles and the different mechanical protection provided by the mineral matrix could lead to the heterogeneity of OM porosity. However, most of the mesopores and all of the micropores could not be quantified due to the limited resolution (pixel size 15 nm) of SEM used by Mathia et al. (2016) and no complementary methods (e.g., gas adsorption and MIP) were conducted to quantitatively characterize the micropores and mesopores, which restricted the acquisition of accurate and complete shale pore structure evolution information to some extent.

Liu et al. (2017) qualitatively and quantitatively characterized the pore structure of Longmaxi Formation shale samples from the Sichuan Baisn in China and proposed a double-pore evolution conceptual model which included both the evolution characteristics of inorganic pores and organic pores based on their own data and the data from previous studies (e.g., Curtis et al., 2012; Wang et al., 2013). This model was different from the aforementioned models and was divided into 5 stages: (1) immature stage with rapid compaction ($R_0 < 0.7\%$): inorganic pores were reduced rapidly by compaction while no significant change occurred for organic pores. (2) mature stage with hydrocarbon generation-dissolution $(0.7\% < R_o < 1.3\%)$: secondary inorganic porosity was increased by dissolution of carbonates and feldspar with the participation of organic acids and organic porosity was also increased by formation of OM pores during hydrocarbon generation. (3) high-mature stage with pore filling $(1.3\% < R_0 < 2.2\%)$: inorganic pores were decreased slowly by compaction and organic porosity was declined by the OM pore filling of bitumen. (4) overmature stage with secondary cracking $(2.2\% < R_0 < 2.7\%)$: inorganic porosity continued to decrease slowly by compaction while organic porosity was increased due to the secondary cracking of OM. (5) overmature stage with slow compaction ($R_0 > 2.7\%$): both the organic and inorganic porosities were reduced slowly by compaction. The correlations between shale porosity and TOC observed by Milliken et al. (2013) were partially supported by Liu et al. (2017), which indicated the important and complicated influence of TOC on shale porosity.

The influence of thermal maturity on shale pore structure was also confirmed by Dong et al. (2019) by using Upper Devonian Duvernay Formation shale samples with a thermal maturity range from immature to dry-gas window from Western Canada Sedimentary Basin. The TOC ranged from 0.1 to 11.3 wt% and the crossplots of HI versus T_{max} indicated the dominant type II OM with a minor contribution of type III terrigeneous OM in these shale samples. N2 adsorption and MIP were used to quantitatively characterize shale pore structure while FE-SEM and helium ion microscopy (HIM) were applied to qualitatively characterize shale pore structure. As mentioned by Wang et al. (2016), HIM had a higher resolution and better imaging results than SEM, which was also confirmed by Dong et al. (2019). The correlations between pore structure (permeability, porosity, pore volume of microopre, mesopore and macropore) and shale compositions (TOC and SiO₂, Al₂O₃, CaO) were investigated in detail. The results showed a positive correlation between porosity and quartz content, a negative correlation between porosity and carbonate content and a weakly positive correlation between permeability and SiO₂ content. And samples with higher thermal maturity tended to have a smaller pore size. Dong et al. (2019) divided the shale pore structure evolution process into three stages based on their samples: (1) from immature to oil window: porosity decreased due to compaction. (2) from oil window to wet-gas window: the formation of secondary OM pores



Fig. 1. Pore structure evolution models proposed by different scholars using natural shale samples with different thermal maturities.

and feldspar dissolution pores, the primary pore preservation by the quartz framework caused the increase of porosity. The critical role of silica nanospheres and microcrystalline quartz on pore preservation was further approved by Dong and Harris (2020). (3) from wet-gas window to dry-gas window: the OM pores and dissolution pores were compacted leading to the porosity decrease. Furthermore, Dong et al. (2019) pointed out the changes of pore type in shale samples with different thermal maturities. The dominant pores developed in immature samples were interparticle pores between clay minerals and other mineral grains while OM fissures were widely distributed in oil-window samples and secondary bubble-like OM pores were well developed in gas-window samples. It could be seen that this shale pore structure evolution model was somewhat different from the previous models proposed by Mastalerz et al. (2013) and Liu et al. (2017), which was closely related to the different shale samples used by these scholars.

By conducting a thorough literature review of shale wettability characterization using spontaneous imbibition experiments, Gao et al. (2019) established a wettability evolution model considering the significant impact of pore structure on

shale wettability. This model was divided into four stages: (1) $0.5\% < R_0 < 1.3\%$: OM pores began to form by primary cracking of OM while inorganic pores were reduced by compaction and oil filling. However, inorganic pores were still the dominant pore type at this stage. (2) $1.3\% < R_o < 2.0\%$: many OM pores were generated by secondary cracking of OM while inorganic pores were further eliminated due to the enhanced compaction. The comparative relationship between inorganic pores and OM pores was not fixed at this stage. (3) 2.0% < R_o< 3.0%: OM pores became the dominant pore type due to the secondary cracking of OM and the massive elimination of inorganic pores by strong compaction. (4) $R_0 > 3.0\%$: OM pores were reduced due to the weakened secondary cracking of OM and strong compaction. It should be noted that this model was empirical and simplified, which required a lot of further studies to verify its validity.

In summary, the abovementioned studies always showed different shale pore structure evolution models (Fig. 1; Table 1), which indicated the strong dependence of these models on used shale samples and the difficulty of obtaining a unified shale pore structure evolution model. However, the controlling

Formation name	Stage	R _o (%)	Pore evolution*	Main factors	Reference
Devonian and Mississippian	stage 1	<0.55%	Decreased a lot	compaction	
	stage 2	$0.55\%{\sim}0.65\%$	Increased a little	primary cracking of OM	Mastalerz et al., 2013
	stage 3	0.65%~1.15%	Decreased	oil filling and bitumen formation	
	stage 4	>1.15%	Increased	secondary cracking of OM	
Longmaxi	stage 1	<0.7%	IP decreased rapidly	compaction	
	stage 2	0.7%~1.3%	IP and OP increased	hydrocarbon generation and disso- lution	
	stage 3	$1.3\%{\sim}2.2\%$	IP and OP decreased	compaction and bitumen filling	Liu et al., 2017
	stage 4	2.2%~2.7%	IP decreased OP increased	compaction and secondary crack- ing of OM	
	stage 5	>2.7%	Decreased slowly	compaction	
Duvernay	immature-oil window	0.5%~1.3%	Total porosity decreased	compaction	
	oil window-wet- gas window	1.3%~2.0%	Micropore and total porosity increased	hydrocarbon generation and disso- lution	Dong et al., 2019
	wet-gas window- dry-gas window	>2.0%	Decreased	compaction	

 Table 1. The shale pore structure evolution stages and controlling factors indicated from natural shale samples with different thermal maturities in the literature.

*IP=Inorganic porosity, OP=Organic porosity

effects of inorganic and organic diagenesis on shale pore structure evolution are widely recognized in the literature.

3. Shale samples with different thermal maturities from thermal simulation experiments

Following the time-temperature compensation principle proposed by Connan (1974), thermal simulation experiments conducted at a consecutive series of high temperatures are considered as a practical method to simulate the long-time low-temperature geological evolution process in a relatively short experimental time. In recent years more and more studies are conducted to reveal the shale pore structure evolution process using thermal simulation experiments.

Anhydrous pyrolysis experiments were conducted on three low maturity shales/mudstones with $\sim 0.60\%~R_o$ and a coal sample with 0.56% Ro by Chen and Xiao (2014). Two organicrich shale samples LCG and DL were collected from an Upper Permian outcrop (Yaomoshan, Urumqi) of the southern Junggar Basin and an Upper Permian outcrop (Changjianggou, Guangyuan) in the northern Sichuan Basin respectively. The organic-lean mudstone sample EP from an Oligocene deposit of well WC19-1M-1 in the western Pearl River Mouth Basin was used to investigate the pore structure evolution characteristics of clay minerals. The purpose of conducting pyrolysis experiment on the coal sample with a similar initial thermal maturity was to indicate the thermal maturity of the shale samples at different pyrolysis temperatures by measuring the thermal maturity of the coal sample at the equivalent pyrolysis temperatures (Waples, 1980; Sweeney and Burnham, 1990). The anhydrous pyrolysis experiments were conducted at temperatures from 300 to 750 °C with 50 °C intervals to obtain a series of simulated samples with a Ro value range from 0.69% to 4.19%. Low-pressure N2 adsorption tests and CO₂ adsorption tests were applied to quantitatively characterize the mesopores and micropores in simulated samples respectively. Samples LCG and DL generally showed similar pore structure evolution characteristics in the whole maturity range with just a little difference occurring in the oil window: the specific surface area and volume of micropores and mesopores for sample LCG arrived at a minimum around the oil window ($R_0 = 0.89\%$) while these parameters of sample DL showed a slight increase in this thermal maturity range. Furthermore, Chen and Xiao (2014) attributed this difference to the oil generation potential difference between these two samples. More specifically, sample LCG had oil-prone kerogen which could produce a lot of asphaltene-rich bitumen causing obvious pore filling and porosity decrease in the oil window stage while sample DL contained gas-prone kerogen which could only generate a small amount of bitumen showing little influence on shale pore structure. However, the surface areas and volumes of micropores and mesopores for sample EP showed a monotonous decreasing trend with increasing thermal maturity due to the dehydration and framework collapse of clay minerals during thermal maturation process. Chen and Xiao (2014) pointed out the opposite tendency of pore structure evolution between OM and clay minerals determined the shale pore structure evolution characteristics. Finally, Chen and Xiao (2014) proposed an OM pore structure evolution model which could be divided into three stages: (1) formation stage of OM-hosted nanopores (0.6% < Ro < 2.0%): OM pores were produced by oil generation and thermal cracking of generated oil. The residual oil rich in asphaltene and resin formed with the migration of generated oil could cause the pore filling and porosity decrease in oil-prone shales within the oil window stage. The nanoporous pyrobitumen produced by oil cracking to gaseous hydrocarbons at higher thermal maturity and residue kerogen made a contribution to the total pore spaces. (2) developing stage of OM-hosted nanopores $(2.0\% < R_0 < 3.5\%)$: OMs with a graphitic-like structure and a large number of nanopores were produced by further thermal cracking of kerogen and pyrobitumen and the secondary cracking of heavy hydrocarbon gases, which caused a rapid increase of pore volume and specific surface area of micropores and mesopores. (3) conversion and destruction stage of OM-hosted nanopores ($R_0 > 3.5\%$): the transformation of micropores to mespores and/or mesopores to macropores was indicated by the decrease of mircoporosity and the increase of mesoporosity under the experimental conditions at this stage. However, OM pores could be compacted under geological conditions. It should be noted that direct FE-SEM observations of shale pore structure and analysis of gaseous products during pyrolysis experiments were not performed by Chen and Xiao (2014). There was no external pressure and no water (or brine) during the pyrolysis experiments, which could not accurately represent the actual geological conditions. Consequently, all these issues impaired the reliability of the OM pore structure evolution model proposed by Chen and Xiao (2014).

Hydrous pyrolysis experiments with controlled lithostatic pressure (100 MPa) and hydrodynamic pressure (50 MPa) were conducted by Sun et al. (2015) using a Triassic Yanchang Formation Chang 7 member oil-shale sample with type I kerogen, a TOC of 13.75% and 0.7% Ro from an outcrop in Ordos Basin of China. The pyrolysis experiments were conducted at temperatures of 250 °C, 300 °C, 350 °C, 375 °C, 400 °C, 450 °C and 500 °C. The expelled oil, washout oil, residue oil and generated gas were collected and measured once the experiment was completed. N₂ adsorption was the only pore structure characterization method used by Sun et al. (2015). The total pore volume, surface area as well as the pore volume and specific surface area of micropores, mesopores and macropores showed an increasing tendency with increasing temperature. In addition, the average pore diameters of macropores and mesopores decreased with increasing temperature. The pore structure evolution process was divided into three stages by Sun et al. (2015): (1) $250 \sim 300$ °C: primary pores were filled by generated hydrocarbons. (2) 350~375 °C: secondary pores were produced by hydrocarbon generation. (3) 400~500 °C: more secondary pores were generated because of thermal cracking of generated oil. It should be noted that the pyrolysis experiments conducted by Sun et al. (2015) were already optimized to reflect the actual geological conditions. However, lacking of direct FE-SEM observations of shale pore structure and the solely application of N₂ adsorption tests to obtain pore structure were the main issues existed in the work of Sun et al. (2015).

Wu et al. (2015) also conducted thermal simulation experiments with high temperature and pressure (90 MPa) on low mature Triassic Yanchang Formation Chang 7 Member shale samples (2452.6 m depth, 0.67% R_o , a TOC of 2.23% and type II kerogen) from the Ordos Basin. The thermal simulation experiments were conducted at three temperature points of 350 °C, 450 °C, 550 °C and the corresponding values of R_0 were 1.0%~1.5%, 2.0%~2.5%, 2.5%~3.0% respectively. Compared with Sun et al. (2015), Wu et al. (2015) realized the direct 'in-situ' observations of shale pore structure evolution by repeatedly conducting Nano-CT or FE-SEM tests on the same sample block which went through all the three temperature points, and provided a possible way to observe shale pore structure evolution directly. Nano-CT results showed the pore-throat size and development level of pores in simulated samples increased rapidly from 350 to 450 °C and increased slowly from 450 to 550 °C. The N2 adsorption results showed an increase trend of BET surface area and pore volume of simulated samples with increasing temperature. Based on their observations, Wu et al. (2015) pointed out thermal evolution of OM made the greatest contribution to shale pore structure evolution, followed by the transformation of clay minerals and the evolution of brittle minerals made the least contribution. The OMs developed in Chang 7 member shale sample were categorized into two types according to their morphology (OM with irregular shapes and microfractures and OM with block shapes and no microfractures) and these two types of OM generally showed similar evolution tendency. As the increase of simulation temperature, OMs were thermally cracked to generate hydrocarbons with the formation of OM pores and finally OMs were completely cracked and evolved into large pores. These two types of OM also showed a little evolution difference. OM with microfractrues generated pore spaces mainly in two forms: the extension of microfretures within OM and the formation of microfractures at the interface between OM and mineral matrix. The pores developed in OM with block shapes were mainly distributed at the interface between OM and mineral matrix due to the shrinkage of OM. With the increase of simulation temperature, the intra-particle pores were gradually generated in I/S mixed layer clay minerals and chlorite. The pore size of intra-particle pores developed in clay minerals increased significantly at 350 °C and did not change a lot after this temperature, which indicated the contribution of transformation of clay minerals to pore spaces was quite limited after the gas-window. The dissolution pores generated by the interaction between unstable minerals (feldspar and calcite) and organic fluids were also observed but their pore size and pore connectivity were not significantly increased with increasing temperature. Finally, Wu et al. (2015) proposed a shale pore structure evolution model which was divided into three stages: (1) $R_0 < 0.5$: the pore system was reduced rapidly due to the mechanical compaction. (2) 350~450 °C: the pore system was increased rapidly due to the formation of OM pores, dissolution pores and intra-particle pores developed in clay minerals. (3) 550 °C: the pore system was kept stable at this stage due to the weak thermal cracking of OM, the enhanced stability of shale framework and the stable fluid environment. Furthermore, Wu et al. (2019) expanded their study to marine Proterozoic Xiamaling Formation shale sample in the North China Platform ($R_0 < 0.7\%$, TOC>2.2%, and type II kerogen) and lacustrine Permian Lucaogou Formation shale sample in the Junggar Basin (Ro<0.7%, TOC>2.2%, and type II kerogen) using similar experimental procedures with Wu et al. (2015). Basically, the results of Wu et al.

(2019) were consistent with those of Wu et al. (2015). One of the main progresses made by Wu et al. (2019) was that an improved shale pore structure evolution model with four stages was proposed by adding a new stage ($250 \sim 300 \,^{\circ}$ C) to the model proposed by Wu et al. (2015). During the stage of $250 \sim 300 \,^{\circ}$ C, inorganic pores were further reduced due to the mechanical compaction while organic pores were increased first due to the pyrolysis of OM and then decreased by the swelling of OM caused by the adsorption and dissolution of generated liquid hydrocarbons in the kerogen framework. It could be seen that the model proposed by Wu et al. (2019) did not show a decreasing trend of porosity during the overmature stage and the highest temperature of 550 $^{\circ}$ C used by Wu et al. (2015) and Wu et al. (2019) was possibly not high enough to reveal a complete shale pore structure evolution process.

Ko et al. (2016) conducted anhydrous gold tube pyrolysis experiments under confining pressure (68.95 MPa) on lowmaturity Upper Cretaceous Boquillas Formation (Eagle Fordequivalent) organic-lean calcareous mudrock samples ($\sim 0.7\%$ R_0 and type II kerogen) from outcrops along US Highway 90, west of Del Rio, Texas. The pyrolysis experiments were conducted at seven temperature points: 130 °C, 300 °C, 310 °C, 333 °C, 367 °C, 400 °C, 425 °C. The shale pore structure evolution characteristics were mainly investigated by geochemical analysis and SEM petrography. Ko et al. (2016) provided the definitions of four different OM pore types categorized by their morphology and origin: primary OM pores, convoluted OM pores, spongy OM pores and shrinkage OM pores. The generation of spongy OM pores was related to the thermal maturation of OM. Primary OM pores were inherited from original OM and convoluted OM pores were produced due to the deformation of OM, both of which were not related to the thermal maturation of OM. The shrinkage OM pores were considered as artifacts formed due to the postexperimental temperature and confining pressure drops. The modified mineral pores with relic OM proposed by Ko et al. (2016) were related to petroleum migration in shale. Ko et al. (2016) also provided the working definitions of OM, kerogen, bitumen, solid (or solidified) bitumen, pyrobitumen, char and residual (or retained) oil in their study. Basically, Ko et al. (2016) divided the shale pore structure evolution process into three stages: Stage I (Bitumen generation; $130 \sim 310$ °C): modified mineral pores were the dominant pore type in this stage. Stage II (Early oil and oil window; 333~367 °C): the spongy OM pores were generated in this stage but the modified mineral pores with isopachous OM rim were still the dominant pore type. Stage III (peak oil generation and cracking of oil to gas; 400~425 °C): the modified mineral pores and nanometer-sized spongy OM pores were the two dominant pore types in this stage. Furthermore, Ko et al. (2016) also evaluated the pore structure of four different types of matrix and the development level of porosity and pore size was in the following order: calcite-dominated matrix>mixed matrix (clay mineral, calcite and quartz)>quartzdominated matrix>clay mineral-dominated matrix. The pore size distribution of different types of matrix was influenced by grain size (Dewhurst et al., 1998, 1999) and could affect the evolution process of mineral pores and OM pores. The overall porosity in the calcite-dominated matrix was lower in the early oil cracking to gas stage compared with bitumen and oil generation stage while the overall porosity in all the other three types of matrix showed an increasing trend with increased thermal maturation. Consequently, depositional and diagenetic (physical compaction and chemical alteration) processes and thermal maturation of OM were considered as the controlling factors of shale pore structure evolution. In addition, Ko et al. (2016) made a pore structure comparison between naturally matured Eagle Ford core samples with calcite-dominated facies and artificially heated Boquillas samples. The main difference was the abundant existence of modified mineral pores in the artificially heated early gas window samples, which was possibly caused by their different mechanisms of petroleum retention. Following the work of Ko et al. (2016), Ko et al. (2018) expanded their investigations of shale pore structure evolution to Upper Devonian-Lower Mississippian Woodford and Mississippian Barnett immature mudstones. Barnett siliceous mudstone with dominant type II kerogen showed similar pore structure evolution characteristics to that proposed by Ko et al. (2016) for Boquillas Formation (Eagle Ford-equivalent) mudstones while Woodford siliceous mudstone with dominant type II kerogen had a different pore evolution history because Woodford mudstone with abundant Tasmanites (telalginite) OM had a later and shorter OM conversion and petroleum generation history. More specifically, the dominant pore types developed in Woodford siliceous mudstone changed from bubble-like OM pores in the early bitumen stage, to few bubble-like OM pores and modified mineral pores in the peak bitumen stage, to increased bubblelike OM pores and modified mineral pores in the early oil stage (Tasmanites OM started to convert to petroleum), to dominant modified mineral pores in the oil window stage (full conversion of Tasmanites OM to petroleum), to most abundant modified mineral pores in the early cracking of oil to wetgas stage. It could be seen that the maceral type could also affect the OM pore structure evolution process. Although the quantification of pore structure by manual pore tracing on two SEM images was presented by Ko et al. (2016), shale pore structure evolution process was still mainly qualitatively described and the quantification of FE-SEM images usually could not provide the complete shale pore structure information due to the limited imaging area and resolution.

Thermal simulation experiments were conducted by Wang and Guo (2019) using Jurassic Yanan Formation shale core samples with a TOC of 2.52%, type III kerogen and 0.5% R_o collected from the western margin of the Ordos Basin. Hydrous pyrolysis experiments were conducted at 10 temperature points from 200 to 650 °C with 50 °C intervals and the amount of hydrocarbons generated at each temperature point was measured. In addition, the shale pore structure of artificially heated samples was characterized qualitatively by FE-SEM and the whole-aperture quantitative pore structure characterization was achieved by combining CO₂ (for micropore), N₂ (for mesopore) and MIP (for macropore). Finally, Wang and Guo (2019) established a shale pore structure evolution model with four stages: (1) R_o \leq 0.7%: Due to compaction, micropores decreased slowly while mesopores, macropores



Fig. 2. Pore structure evolution models proposed by different scholars using thermal simulation experiments.

and total pores were reduced rapidly. (2) $0.7\% \le R_0 \le 1.6\%$: The hydrocarbon generation by OM controlled the pore structure evolution in this stage. The total pores decreased rapidly first and reached a minimum at 0.78% Ro and then increased slowly. More specifically, micropores and mesopores showed similar changing trend with total pores while macropores increased slowly during this stage. The rapid decrease of micropores was caused by the infilling of bitumen generated from kerogen pyrolysis and the later increase of mircopores was because of the cracking of bitumen and the release of hydrocarbon. The decrease of mesopores was caused by both compaction and bitumen infilling. The dissolution of unstable minerals (e.g., feldspar) by organic acids produced during the thermal evolution of OM and the shrinkage cracks formed during hydrocarbon generation caused the increase of mesopores and macropores. High pore pressures generated by hydrocarbon generation and thermal cracking of hydrocarbons in the subsurface could resist compaction and might be another reason for the increase of mesopores and macropores. (3) $1.6\% \le R_0 \le 2.3\%$: The hydrocarbon generation by OM and the transformation of clay minerals controlled the pore structure evolution in this stage. The micorpores decreased first and then increased while the mesopores increased first and then decreased. The macropores increased rapidly and the total pores increased steadily. The decrease of micropores was caused by the combination of micropores to mesopores and the later increase of micropores was due to the solid bitumen with abundant micropores generated by kerogen polycondensation in this stage. The combination of micropores, the illitization, the shrinkage of smectite due to dehydration and the

dissolution caused the first increase of mesopores. The later decrease of mesopores was caused by the combination of mesopores into macropores. The increase of macropores was caused by the combination of mesopores into macropores, the illitization, the shrinkage of smectite due to dehydration and the dissolution. (4) $R_0 \ge 2.3\%$: The total pores increased to the maximum value and then decreased due to pore blockage during the aggravation of kerogen aromatization and the pore collapse under the increasing external pressure.

Although not exactly modeling the shale pore structure evolution process under geological conditions with lower temperature, very long time period and complicated geofluid systems, thermal simulation experiment is still a practical method to obtain a series of shale samples with same compositions and different maturities in the laboratory. However, the proposed shale pore structure evolution models are largely dependent on the used shale samples and the experimental conditions (Fig. 2; Table 2). It is unrealistic to conduct lots of thermal simulation experiments on shale samples with many lithofacies due to the high cost of thermal simulation experiments.

4. Conclusion

Thermal evolution of OM includes hydrocarbon generation, migration and thermal cracking of hydrocarbon. The primary and secondary cracking of OM could increase the OM pore spaces while the pore filling of generated bitumen may lead to the decrease of inorganic and OM pore spaces. Different types of kerogen always show different hydrocarbon generation history during thermal maturation and then lead to different

Formation name	Experimental conditions	Stage	Pore evolution	Main factors	Reference	
Upper Permian outcrop; Oligocene deposit		0.6% <ro<2.0%< td=""><td>pore volume decreased and then increased</td><td>oil generation and thermal cracking; pore filling in oil-prone shales</td><td></td></ro<2.0%<>	pore volume decreased and then increased	oil generation and thermal cracking; pore filling in oil-prone shales		
	anhydrous; $300 \sim 750 ^{\circ}\text{C}$;	$2.0\%{<}R_o{<}3.5\%$	pore volume increased rapidly	thermal cracking of kerogen	Chen and Xiao, 2014	
	$(\mathbf{R}_0, 0.09\%, 0.09\%)$	R _o >3.5%	microporosity decreased and mesoporosity increased	conversion and destruction of OM pores		
Yanchang Formation	bydrous: 250, 500 °C.	250~300 °C	primary pores were filled	hydrocarbon generation		
	lithostatic pressure: 100 MPa,	350~375 °C	secondary pores were produced	hydrocarbon generation	Sun et al., 2015	
	hydrodynamic pressure: 50 MPa	400~500 °C	more secondary pores were produced	thermal cracking		
Yanchang Formation; Xiamaling Formation; Lucaogou Formation	350∼550 °C; 70, 80, 90 MPa	R _o <0.5%	decreased rapidly	compaction	Wu et al., 2015, 2019	
		250~300 °C	IP decreased; OP increased and then decreased	compaction; hydrocarbon generation		
		350~450 °C	increased rapidly	formation of OM pores, dissolution pores, clay mineral pores		
		550 °C	stable	weak thermal cracking of OM, the enhanced stability of shale framework and the stable fluid environment		
Boquillas Formation	anhydrous; 130~425 °C; 68.95 MPa	130~4310 °C	modified mineral pores were the dominant pore type	bitumen generation	Ko et al., 2016	
		333~367 °C	the spongy OM pores increased but the modified mineral pores and primary IP decreased	early oil and oil window		
		400~425 °C	the modified mineral pores and nanometer-sized spongy OM pores were dominant pore types	peak oil generation and cracking of oil to gas		
Yanan Formation	hydrous; 200~650 °C	$R_o \leq 0.7\%$	micropores decreased slowly while mesopores, macropores and total pores reduced rapidly	compaction	Wang and Guo, 2019	
		$0.7\% \le R_o \le 1.6\%$	micropores, mesopores and total pores decreased rapidly and then increased slowly; macropores increased slowly	hydrocarbon generation; dissolution; shrinkage cracks		
		$1.6\% \le R_o \le 2.3\%$	micropore decreased and then increased; mesopore increased and then decreased; macropores and total pores increased	hydrocarbon generation; formation of solid bitumen; transformation of clay minerals		
		$R_o \ge 2.3\%$	total pores increased and then decreased	pore blockage and collapse.		

Table 2. The shale pore structure evolution stages and controlling factors indicated from thermal simulation experiments in the literature.

pore structure evolution characteristics. In addition, Lohr et al. (2015) observed the common existence of primary OM pores in immature shale samples, which depended on the OM type and affected the following OM pore development at higher thermal maturities. Consequently, the OM pores were not only generated by thermal evolution of OM but also could be inherited from their parent OM. However, few studies have been conducted to investigate the pore structure evolution process of different types of OMs.

Inorganic diagenesis mainly consists of compaction, dissolution, and transformation of clay minerals. And the mineral composition of shale significantly affects inorganic diagenesis. Compaction decreases pore spaces significantly during the immature stage and continues to decrease pore spaces during the whole evolution process at different levels. Dissolution of unstable minerals by generated organic fluids creates new pore spaces. However, the role of transformation of clay minerals in pore structure evolution is still disputable, which requires more investigations.

Consequently, the inorganic and organic diagenesis simultaneously control the shale pore structure evolution process, which complicates the revealing of shale pore structure evolution. Furthermore, Liu et al. (2017) discussed the influence of tectonic characteristics on shale pore structure, which expanded the research content of shale pore structure evolution to a larger scale and requires more targeted investigations. Pore structure comparison of a series of natural shale samples with different thermal maturities and similar shale compositions using quantitative (mainly CO2 adsorption, N2 adsorption, MIP) and qualitative (mainly FE-SEM) pore structure characterization instruments is commonly used to investigate shale pore structure evolution characteristics. However, due to the strong heterogeneity of shale and complicated diagenesis, minor difference in shale compositions may cause quite different evolution characteristics, which makes the reliability of this method dependent on the accurate selection of shale samples.

Obtaining a series of shale samples with different thermal maturities using thermal simulation experiments could resolve the issue of shale composition difference. It should be noted that investigating shale pore structure evolution by statistical comparison of FE-SEM images of different sample blocks is somewhat subjective due to the limited imaging areas of FE-SEM and the representative issue of used images. In order to avoid this problem, the 'in-situ' observation method of pore structure evolution proposed by Wu et al. (2015) is a relatively ideal way to show the pore structure evolution process directly. However, it is almost impossible to set up thermal simulation experimental conditions exactly same with the real underground conditions (e.g., complicated geofluid systems), which is the main weakness of this method. Consequently, it is better to combine these two methods together in order to obtain more reliable shale pore structure evolution characteristics in future investigations. As the imaging resolution significantly affects the shale pore structure characterization result, the imaging instruments with higher resolution (≤ 1 nm) should be developed and applied in future studies.

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Conflict of interest

The authors declare no competing interest.

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